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Multi products single machine EPQ model with immediate rework process

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ABSTRACT

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Keywords: Economic production quantity Rework process Limited production capacity This paper develops an economic production quantity (EPQ) inventory model with rework process for a single stage production system with one machine. The existence of a unique machine results in limited production capacity. The aim of this research is to determine both the optimal cycle length and the optimal production quantity for each product to minimize the expected total cost (holding, production, setup, rework costs). The convexity of the inventory model is derived. Also the objective function is proved to be convex. The proposed inventory model is validated with illustrating numerical examples and the optimal period length and the total system cost are analyzed.

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1. Introduction

Raw material is considered as one of the main issues for any manufacturing process. The management of material begins by the regulation of the flow of the raw materials which enters to organization till they are changed into final products. An efficient strategy on raw materials could lead to higher revenue growth and profitability. During the past few decades, there have been tremendous efforts to adapt globalization by obtaining resources from different regions of the world. Therefore, we may expect to use several resources to source and distribute both raw materials and finished goods. In this direction, the key success is to maintain a high level of customer satisfaction. In other word, any disruption in service delivery may lead to lose market share. As a result, inventory management, production planning and scheduling play an important role especially for world class manufacturers.

In manufacturing companies, when products are internally manufactured instead of being obtained from an outside vendor, the economic production quantity (EPQ) inventory model is frequently employed to calculate the optimal lot size minimizing the overall production/inventory costs. One

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primary assumption with any EPQ inventory model is that the products are manufactured perfectly and there is no need of a rework process. However, due to process deterioration, one may end up having imperfect quality items. Therefore, we may attempt to reduce the total production/inventory expenditures by repairing the defective items. There are good examples of the rework processes for example: printed circuit board assembly in the PCBA manufacturing, metal components, and plastic injection molding, just to name a few. Cheng (1991) develops an order quantity inventory model for imperfect production processes when production cost is a function of demand. Chiu et al. (2003) propose a economic production quantity inventory model when scrap items are taken into consideration. Chung (1997) determines some bounds for production lot sizing with machine breakdown.

The economic production cycles with imperfect production processes are studied by Rosenblatt and Lee (1986) and Lee and Rosenblatt (1987); where a manufacturing process can shift from a normal condition to an out-of-control condition. Hayek and Salameh (2001) propose an optimal operating policy for the finite production model with reworking and imperfect quality items. In their inventory model, any defective item could be repaired and backorders are permitted. Rework and breakdown are considered significantly in variety forms (Chiu (2003), Chiu (2007) and Chiu et al. (2007)). Jamal et al. (2004) present a new method when production lot-sizing were faced with imperfect maintenance. Cárdenas-Barrón (2007) corrects the solutions to examples in Jamal et al. (2004) and Cárdenas-Barrón (2008) derives in a simple way the Jamal et al. (2004)'s two inventory policies. The EPQ with rework process and planned backorders can be found in Cárdenas-Barrón (2009a). The multi-stage production system with rework consideration is dealt in Sarker et al. (2008) and Cárdenas-Barrón (2009b).

Chan et al. (2003) study the traditional EPQ with an integrated model with rework and reject items. Chiu and Chiu (2003) study optimal replenishment policy for an imperfect quality EPQ inventory model with backlogging and failure. They derive the optimal lot size using the classical optimization approach based on differential calculus. Islam and Roy (2006) formulate a fuzzy form of EPQ model by considering flexible and reliable production process. Bayindir et al. (2007) develop a new EPQ model with general inventory cost rate function and piecewise linear concave production costs. Hou (2007) investigate an EPQ model with setup cost and process quality as a function of capital expenditure. Then, he develops an efficient procedure to obtain the optimal production run time, setup cost, and process quality. Chiu et al. (2007) study an EPQ inventory model with scrap, rework, and stochastic machine breakdowns. Their inventory model determines both the optimal run time and production lot size. In a subsequent paper, Chiu (2008) develops an optimal solution for the same problem where no information of the derivates was needed. Li et al. (2008) study an EPQ inventory model with planned backorders to evaluate the impact of the postponement strategy on a manufacturer in a supply chain.

Pentico et al. (2009) extend the EPQ inventory model with partial backordering when production lot size and period length are also considered. Teng and Chung (2009) develop another EPQ inventory model under two levels of trade credit policy to optimize the production quantity and period length. Chiu et al. (2004) consider the effects of random defective rate and imperfect rework process on EPQ inventory model. Wee et al. (2007) present an inventory model for items with imperfect quality and shortage backordering. Taleizadeh et al. (2010a) present economic production quantity model with scrapped items and limited production capacity. At the same time, Taleizadeh et al. (2010b) introduce multi-product single-machine production system with stochastic scrapped production rate, partial backordering and service level constraint. Taleizadeh et al. (2010c) also develop a multi product single machine EPQ model with failure and rework when partial backordering exists. In two subsequent research works, Taleizadeh et al. (2011a) extend a multi product single machine EPQ inventory model with multiple batch sizes and Taleizadeh et al. (2011b) develop an extended a multi product single machine EPQ inventory model.

This paper is organized as follows. Section 2 develops the EPQ inventory model with rework process for a single stage production system with one machine. Section 3 presents the solution procedure to solve the optimization problem. Section 4 solves numerical examples and presents a sensitivity analysis. Finally, some conclusions and future researches are given in Section 5.

2. Modeling and formulation

The EPQ inventory model with two kinds of rework processes was considered by Jamal et al. (2004). Their models determine the optimum batch quantity in a single-stage system in which the rework is performed under two different operational policies to minimize the total system cost. An inventory model for a single-stage production system with fraction defective and rework process facility involves various types of cost functions such as setup cost, processing cost, inventory carrying cost, in-process inventory carrying cost for reworking, and penalty cost for defective items. In this paper, we develop the model of Jamal et al. (2004) by considering multi products single machine system with capacity limitation. In fact the existence of a unique machine results in limited production capacity. In this research, we assume demands of each product are constant over the production planning period.

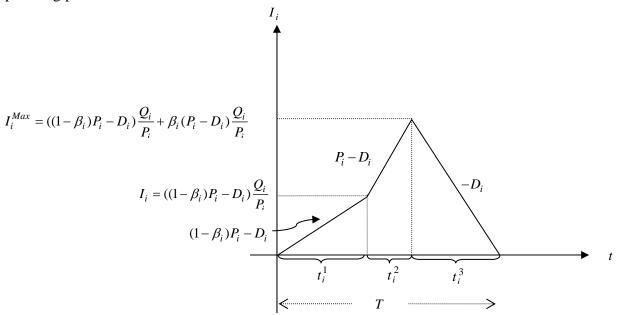


Fig. 1. On hand inventory of perfect quality items

Proportion of defective of each product is constant in each cycle and production rate of non-defective items is constant and is greater than the demand rate of each product. Scrap is not produced at any cycle and no defectives are produced during the rework process. Production and rework are accomplished using the same resource at the same speed and shortage is not allowed. A real constant production capacity limitation on a single machine in which all products are produced and that the setup cost is considered nonzero. Since all products are manufactured and reworked on a single machine with a limited capacity, the cycle length for all of them is equal $(T_1 = T_2 = \cdots = T_n = T)$. Since the problem at hand is of multiproduct with products $i = 1, 2, \cdots, n$, the following notations are used:

 Q_i : Production lot size of i^{th} product for each cycle (Decision variables);

T : Cycle length (Decision variable);

 P_i : Production rate of i^{th} product for each cycle;

 D_i : Demand rate of i^{th} product;

 β_i : Proportion of defective s of i^{th} product in each cycle;

 A_i : Setup cost for each production run of i^{th} product;

 S_i : Setup time of machine to produce the i^{th} product;

N: Number of cycles per year;

TC: Total inventory costs per year;

 I_i : Maximum level of on-hand inventory of i^{th} product when regular production process stops;

 I_i^{Max} : Maximum level of on-hand inventory of i^{th} product in units, when the reworking ends;

 C_i^P : Production cost of i^{th} product, \$/item;

 C_i^h : Holding cost of i^{th} product per item per unit time, \$\frac{1}{2}\$ item/unit time.

2.1. Formulation

Initially the problem is modeled as a single product case and then it is modified as a multi product case. The basic assumption of EPQ model with rework process produced is that P_i must always be greater than or equal to the sum of demand rate D_i . Therefore we have:

$$((1-\beta_i)P_i - D_i) \ge 0. \tag{1}$$

The production cycle length (see Fig. 1) is the summation of the production uptime, the reworking time and the production downtime:

$$T = \sum_{i=1}^{3} t_i^j, (2)$$

where the production uptime (including healthy and defective items) is t_i^1 , the reworking time is t_i^2 and the production downtime is t_i^3 . To model the problem, a part of the modeling procedure is adopted from Jamal et al. (2004). Since all products are manufactured on a single machine with a limited capacity, the cycle length for all of them are equal $(T_1 = T_2 = \cdots = T_n = T)$. Then, based on Fig. 1, for $i = 1, 2, \dots, n$, we have:

$$t_i^1 = \frac{Q_i}{P_i},\tag{3}$$

$$t_i^2 = \beta_i \frac{Q_i}{P_i},\tag{4}$$

$$t_i^3 = \frac{\left(1 - \frac{D_i}{P_i} - \beta_i \frac{D_i}{P_i}\right) Q_i}{D_i}.$$
(5)

It is evident from Fig. 1 that:

$$I_{i} = ((1 - \beta_{i})P_{i} - D_{i})\frac{Q_{i}}{P_{i}},$$
(6)

$$I_i^{Max} = I_i + \beta_i (P_i - D_i) \frac{Q_i}{P_i} = ((1 - \beta_i) P_i - D_i) \frac{Q_i}{P_i} + \beta_i (P_i - D_i) \frac{Q_i}{P_i}.$$
(7)

Hence, according to Eq. (2) the cycle length for a single product state is:

$$T = \sum_{i=1}^{3} t_i^j = \frac{Q_i}{D_i}.$$
 (8)

or,

$$Q_i = D_i T. (9)$$

The total production cost of the system consists of setup cost, processing cost, rework cost and inventory carrying costs. Defective items are produced in every batch and they are reworked within the same cycle. During the rework of defective items, again some processing costs and inventory holding costs are incurred for processing and holding the reworked quantities as well. The total inventory cost per year *TC* is:

$$TC = NC_{i}^{P}Q_{i} + NA_{i}^{Cost} + NC_{i}^{P}\beta_{i}Q_{i} + NC_{i}^{h}\left[\frac{I_{i}}{2}(t_{i}^{1}) + \frac{I_{i} + I_{i}^{Max}}{2}(t_{i}^{2}) + \frac{I_{i}^{Max}}{2}(t_{i}^{3})\right].$$

$$(10)$$

The joint production policy (Multi-Product Single-Machine) from Eq. (10) becomes:

$$TC = \sum_{i=1}^{n} C_{i}^{P} D_{i} + \frac{\sum_{i=1}^{n} A_{i}}{T} + \sum_{i=1}^{n} C_{i}^{P} \beta_{i} D_{i} + \sum_{i=1}^{n} C_{i}^{h} \left[\frac{I_{i}}{2T} (t_{i}^{1}) + \frac{I_{i} + I_{i}^{Max}}{2T} (t_{i}^{2}) + \frac{I_{i}^{Max}}{2T} (t_{i}^{3}). \right]$$

$$(11)$$

2.2. The constraint

Since $t_i^1 + t_i^2$ are the production and rework times and S_i is the setup time for i^{th} product, the summation of the production, rework and setup time (for all products) will be $\sum_{i=1}^{n} (t_i^1 + t_i^2) + \sum_{i=1}^{n} S_i$, and it must be smaller or equal to the period length (T). Therefore, the constraint of the model is:

$$\sum_{i=1}^{n} (t_i^1 + t_i^2) + \sum_{i=1}^{n} S_i \le T.$$
(12)

Then, based on the Eq. (3), (4) and (9), we have:

$$\sum_{i=1}^{n} (1+\beta_i) \frac{D_i}{P_i} T + \sum_{i=1}^{n} S_i \le T.$$
(13)

2.3. Final Model

From Eq. (9), Eq. (11) and Eq. (13), TC in Eq. (11) and constraint in Eq. (13), one can formulate the optimization problem as:

$$\min: TC = \frac{\sum_{i=1}^{n} A_{i}}{T} + \sum_{i=1}^{n} C_{i}^{h} \left[\left[(1 - \beta_{i}) P_{i} - D_{i} \right] \frac{D_{i}}{2P_{i}} + \beta_{i} \left[P_{i} - D_{i} \right] \frac{D_{i}}{P_{i}} \right] \left(1 - \frac{D_{i}}{P_{i}} - \beta_{i} \frac{D_{i}}{P_{i}} \right) T^{2} + \sum_{i=1}^{n} C_{i}^{P} \beta_{i} D_{i} + \sum_{i=1}^{n} C_{i}^{h} \left((1 + \beta_{i}) \left[(1 - \beta_{i}) P_{i} - D_{i} \right] \frac{D_{i}}{2P_{i}} + \beta_{i}^{2} \left[P_{i} - D_{i} \right] \frac{D_{i}}{P_{i}^{2}} \right) T + \sum_{i=1}^{n} C_{i}^{P} D_{i}$$

$$(14)$$

subject to:
$$T \ge \frac{\sum_{i=1}^{n} S_i}{\left[1 - \sum_{i=1}^{n} (1 + \beta_i) \frac{D_i}{P_i}\right]} = T_{Min}$$
(15)

3. Solution method

In order to derive the optimal solution of the final model, a proof of the convexity of the objective function is provided. A classical optimization technique using partial derivatives is performed to derive the optimal solutions.

Theorem1. The objective function TC in Eq. (14) is convex.

Proof: To proof the convexity of TC = Z, the first and second derivatives of objective function are calculated as below:

$$\frac{\partial TC}{\partial T} = -\frac{\sum_{i=1}^{n} A_{i}}{T^{2}} + 2\sum_{i=1}^{n} C_{i}^{h} \left[\left[(1 - \beta_{i}) P_{i} - D_{i} \right] \frac{D_{i}}{2P_{i}} + \beta_{i} \left[P_{i} - D_{i} \right] \frac{D_{i}}{P_{i}} \right] \left(1 - \frac{D_{i}}{P_{i}} - \beta_{i} \frac{D_{i}}{P_{i}} \right) T + \sum_{i=1}^{n} C_{i}^{h} \left((1 + \beta_{i}) \left[(1 - \beta_{i}) P_{i} - D_{i} \right] \frac{D_{i}}{2P_{i}} + \beta_{i}^{2} \left[P_{i} - D_{i} \right] \frac{D_{i}}{P_{i}^{2}} \right) \tag{16}$$

$$\frac{\partial^{2}TC}{\partial T^{2}} = \frac{2\sum_{i=1}^{n} A_{i}}{T^{3}} + 2\sum_{i=1}^{n} C_{i}^{h} \left[\left[(1 - \beta_{i}) P_{i} - D_{i} \right] \frac{D_{i}}{2P_{i}} + \beta_{i} \left[P_{i} - D_{i} \right] \frac{D_{i}}{P_{i}} \right] \left(1 - (1 + \beta_{i}) \frac{D_{i}}{P_{i}} \right) \ge 0$$
(17)

Since the second derivative is non-negative so the objective function is convex and to obtain the optimal solution we have:

$$aT^{3} + bT^{2} + c = 0 ag{18}$$

In which,

$$a = 2\sum_{i=1}^{n} C_{i}^{h} \left[((1 - \beta_{i})P_{i} - D_{i}) \frac{D_{i}}{2P_{i}} + \beta_{i} (P_{i} - D_{i}) \frac{D_{i}}{P_{i}} \right] \left(1 - \frac{D_{i}}{P_{i}} - \beta_{i} \frac{D_{i}}{P_{i}} \right) \ge 0$$

$$(19)$$

$$b = \sum_{i=1}^{n} C_{i}^{h} \left((1 + \beta_{i})((1 - \beta_{i})P_{i} - D_{i}) \frac{D_{i}}{2P_{i}} + \beta_{i}^{2}(P_{i} - D_{i}) \frac{D_{i}}{P_{i}^{2}} \right) \ge 0$$
(20)

$$c = -\sum_{i=1}^{n} A_i \le 0 \tag{21}$$

The solution of Eq. (18) is being obtained numerically by any numeric method such as Newton-Raphson. To solve and ensure the feasibility, the following solution procedure must be performed:

Solution procedure:

Step1. Check for feasibility,

If
$$\sum_{i=1}^{n} (1+\beta_i) \frac{D_i}{P_i} \le 1$$
 and $[(1-\beta_i)P_i - D_i] \ge 0$, go to step 2, else the problem will be infeasible,

Step2. Calculate T using numeric method. If $T \ge 0$, go to step 3, else the problem will be infeasible,

Step3. Calculate by T_{Min} Eq. (15),

Step4. If
$$T \ge T_{Min}$$
 then $T^* = T$ else $T^* = T_{Min}$,

Step5. Calculate Q_i^* by Equation (9),

Step6. Terminate procedure.

4. Numerical examples and sensitivity analysis

4.1. Numerical Example

Consider two multi-products EPQ problems with breakdown and immediate rework with five products in which their general and specific data are given in Table 1 and Table 2, respectively. Tables 3 and Table 4 show the best results for the two numerical examples. For the first example, since the value of T is greater than T_{Min} the 4^{th} step of the procedure implies the optimality of T. However, in the second example we chose T_{Min} as the optimal solution since T is less than T_{Min}

Table 1General data for the first example

		THE CHILIPT					
Product	D_i	P_{i}	S_{i}	A_{i}	C_i^P	C_i^h	$oldsymbol{eta}_i$
1	400	3500	0.003	500	15	5	0.1
2	500	4000	0.004	450	12	4	0.2
3	600	4500	0.005	400	10	3	0.3
4	700	5000	0.006	350	8	2	0.4
5	800	5500	0.007	300	6	1	0.5

Table 2General data for the second example

Product	D_{i}	P_{i}	S_{i}	A_{i}	C_i^P	C_i^h	$oldsymbol{eta}_i$
1	400	3000	0.003	500	15	5	0.1
2	500	3500	0.004	450	12	4	0.2
3	600	4000	0.005	400	10	3	0.3
4	700	4500	0.006	350	8	2	0.4
5	800	5000	0.007	300	6	1	0.5

Table 3The best results for the first example

	110 0000 1000000 101 010 1100 010000							
Product	Uniform	Uniform						
	T_{Min}	T	T^*	Q_i	Z			
1				216.3492				
2				270.4366				
3	0.1827879	0.5408731	0.5408731	324.5239	42998.16			
4				378.6112	_			
5				432.6985				

Table 4The best results for the second example

Product	Uniform						
	$T_{\it Min}$	T	T^*	Q_i	Z		
1				343.3243			
2				429.1553	_		
3	0.8583106	0.5496333	0.8583106	514.9864	43955.41		
4				600.8174	_		
5				686.6485			

4.2. Sensitivity Analysis

To study the effects of the parameter changes on the optimal solutions derived by the proposed method, this investigation performs a sensitivity analysis by increasing or decreasing the parameters, one at a time, by 20% and 50%. Section 4.1 gives two numerical examples, and section 4.2 gives the sensitivity analyses. Tables 5 and 6 show the results of the sensitivity analysis for examples 1 and 2, respectively.

Table 5Effects of Parameter Changes for the First Example

% Changes in parameters and their values		% Changes in				
		T_{Min}	T	T^*	Z	
	+50	-67.78	-6.33	-6.33	+0.86	
P_{i}	+20	-51.27	-3.27	-3.27	+0.43	
l	-20	Infeasible	-	=	-	
	-50	Infeasible	-	=	-	
	+50	0	+31.18	+31.18	+3.35	
A_{i}	+20	0	+13.15	+13.15	+1.39	
ı	-20	0	-14.36	-14.36	-1.47	
	-50	0	-39.07	-39.07	-3.91	
	+50	Infeasible	-	=	-	
D_{i}	+20	Infeasible	-	=	-	
ı	-20	-55.08	+11.76	+11.76	-18.18	
	-50	-75.94	+43.56	+43.96	-46	
	+50	+299.98	+4.18	+103.04	+8.25	
$oldsymbol{eta}_i$	+20	+42.85	+1.37	+1.37	+3.54	
, ,	-20	-23.08	-1.02	-1.02	-3.59	
	-50	-42.86	-1.87	-1.87	-9.07	
	+50	+50	0	0	0	
S_{j}	+20	+20	0	0	0	
	-20	-20	0	0	0	
	-50	-50	0	0	0	

As we have already explained, T^* can be found either directly using numeric method proposed in earlier or it can be obtained from the lower bound. However, in the case of example, some change on P_i forces the optimality to be calculated by the lower bound and we experience significant changes on T^* . We have similar experience between D_i and T^* . In fact T^* is very sensitive to the changes of parameters D_i and P_i . In examples (1) and (2) when P_i is decreased or D_i is increased, the problems become infeasible (See Table 5 and Table 6). The other observation is that when we assign different values for D_i and P_i , T_{Min} becomes negative which means feasible solutions. In the first example T^* is obtained from numeric method, which means that satisfies the lower bound (capacity limitation). However, when β_i is increased by +50 percents, the value of numeric method is changed and it does not satisfy the lower bound which means that T_{Min} needs to be considered as the optimal values of T and the changes values of T^* are greater than 100 percents. The following summarizes our experimental results.

- T_{Min} is highly sensitive to the changes in the values of parameters P_i , D_i , β_i and S_i . Also T_{Min} is also insensitive to the changes in the values of parameter A_i .
- T is slightly sensitive to the changes in the values of P_i and β_i , highly sensitive to the changes in the values of parameters D_i and A_i . Also T is insensitive to the changes in the values of parameter S_i .

• Z is slightly sensitive to the changes in the values of parameters P_i , A_i , β_i and S_i and it is highly sensitive to the changes in the values of parameter D_i .

Table 6Effects of parameter changes for the second example

% Changes in parameters and their values		% Changes in				
		T_{Min}	T	T^*	Z	
	+50	-91.74	-7.26	-60.04	+0.13	
P_{i}	+20	-84.75	-3.76	-58.54	-0.35	
ı	-20	Infeasible	-	-	-	
	-50	Infeasible	=	-	-	
	+50	0	+31.16	0	+2.65	
A_{i}	+20	0	+13.15	0	+1.06	
ı	-20	0	-14.33	0	-1.06	
	-50	0	-39.03	0	-2.67	
	+50	Infeasible	=	-	-	
D_{i}	+20	Infeasible	-	-	-	
ι	-20	-86.96	+11.08	-52.14	-18.82	
	-50	-94.34	+41.47	-39.05	-46.37	
	+50	Infeasible	-	-	-	
$oldsymbol{eta}_i$	+20	Infeasible	=	-		
, ,	-20	-61.14	-1.16	-57.42	-4.39	
	-50	-79.73	-2.23	-57.87	-9.82	
S_{j}	+50	+50	0	+50	+8.14	
	+20	+20	0	+20	+2.74	
	-20	-20	0	-20	-1.85	
	-50	-50	0	-50	-1.78	

5. Conclusions and future researches

This study developed an EPQ model with production capacity limitation and breakdown with immediate rework. The primary aim of this research has been to determine the optimal period lengths and lot sizes for each product. The objective function of the proposed mathematical model has been proved to be convex. Two numerical examples are used to illustrate the implementation of our proposed method and sensitivity analysis has been performed to show the applicability of the proposed methodology. The study provided managerial insights for practitioners in designing an EPQ inventory model with breakdown and immediate rework. Future research could focus on backordered or partial backordering strategies and multi-product multi-constraint problems in an uncertain environment and also explore the problem when the lot sizes are restricted to be integers.

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